

# Reinhold Environmental Ltd.

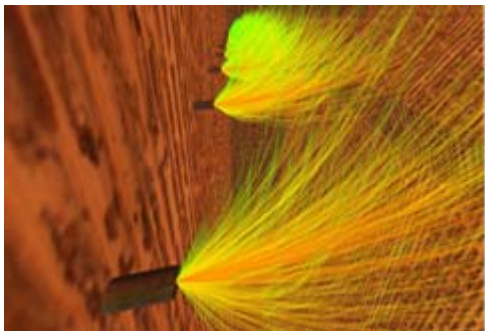


## 2010 NO<sub>x</sub>-Combustion Round Table & Expo Presentation

***February 8 & 9, 2010***

***Chattanooga, TN***

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# 2010 NO<sub>x</sub>- Combustion/PCUG Conference

## Hybrid In-Duct Advanced SCR Technologies

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*Fuel Tech, Inc.*  
*January 30, 2010*

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*January 30, 2010*

# Agenda

- Fuel Tech Introduction
- Advanced SCR Basics
- ASCR Design
- Discussion

# Fuel Tech Overview

- FUEL CHEM<sup>®</sup> Technology –
  - Slag and Corrosion Reduction with Efficiency Improvements
- NO<sub>x</sub> Reduction Technologies
  - LNB / OFA
  - SNCR – “NOx-OUT<sup>®</sup> and HERT<sup>®</sup>”
  - Advanced SCR – the Right Combination of Technologies to Suit Individual Needs
- Services
  - Fluid Dynamics Modeling and Optimization Studies of APC Equipment
  - SCR Consulting and Catalyst Management Services

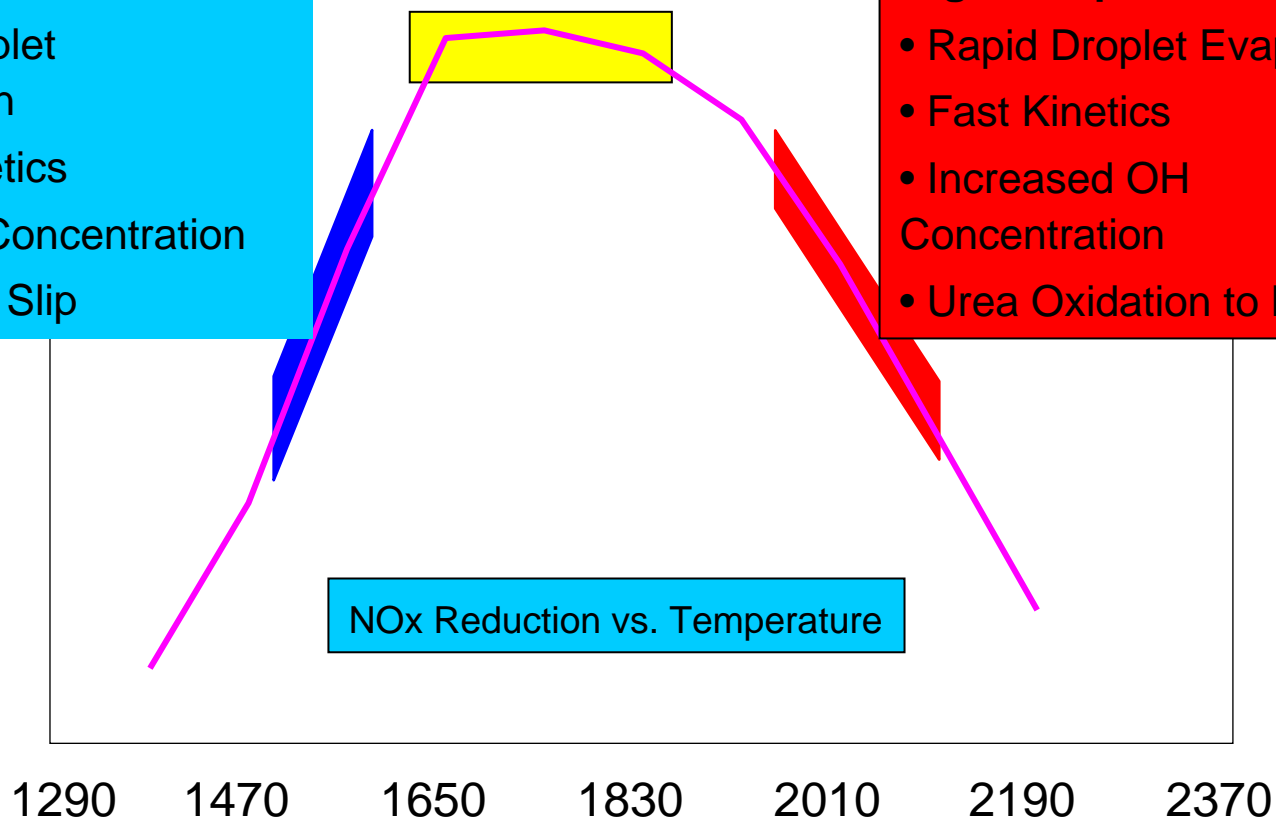
# NO<sub>x</sub> Reduction Technologies - SNCR

## Low Temperatures

- Slow Droplet Evaporation
- Slow Kinetics
- Low OH Concentration
- Ammonia Slip

## High Temperatures

- Rapid Droplet Evaporation
- Fast Kinetics
- Increased OH Concentration
- Urea Oxidation to NO<sub>x</sub>



- 25-60% NO<sub>x</sub> Reduction

# NO<sub>x</sub> Reduction Technology - ASCR

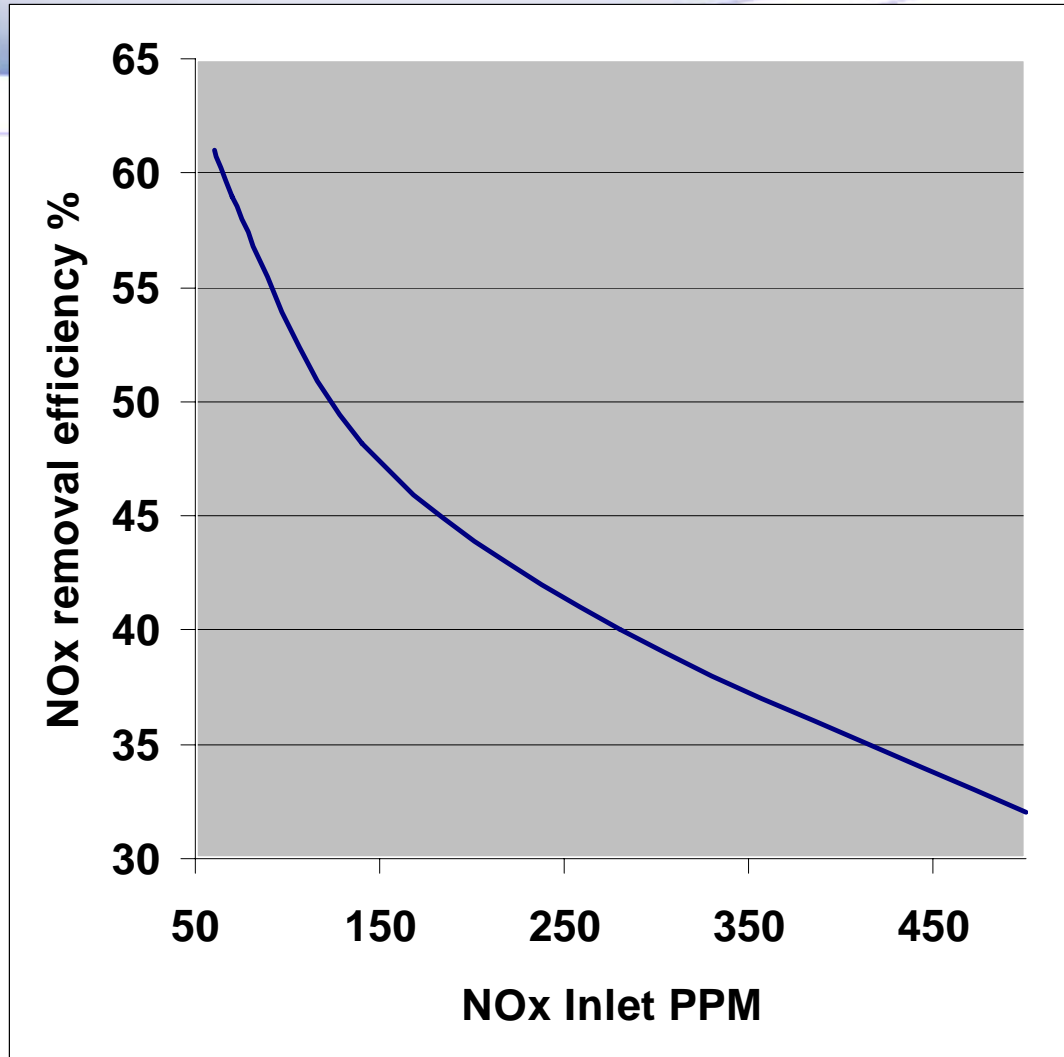


- Layered Technologies of LNB/OFA/SNCR/SCR as Needed
- Single Layer SCR Catalyst
  - No need to “Go to Ground”
- Ammonia Slip from SNCR Provides Reagent for Catalytic Reactions
- Or Additional AIG
- NO<sub>x</sub> Reduction Performance - 50-90%
- Lower Capital Cost compared to Full Scale SCR



# NO<sub>x</sub> Reduction Technology - ASCR

Catalyst Performance



# ASCR/SCR Cost Comparison

- Capital Cost
  - Very Limited Steel Structure
  - Less Catalyst
  - Less Duct Work
- O&M Cost
  - More Catalyst Replacement
  - More Reagent Consumption in SNCR
  - Less Pressure Drop
- Lower Total Cost Except For Very High Capacity Factors
- Break-Even Point Site Limited

# Catalyst Consumption

- SCR For 600 MW Unit 85 %  
Reduction 20 Years Life
  - 600 m<sup>3</sup> Initial Loading
  - 200 m<sup>3</sup> Addition
  - 5 x 200 m<sup>3</sup> Exchange
  - Total Catalyst Demand 1,800 m<sup>3</sup>
  - NPV \$7,426,000
- ASCR For 600 MW Unit 85 %  
Reduction 20 Years Life
  - 200 m<sup>3</sup> Initial Loading
  - 9 x 200 m<sup>3</sup> Exchange
  - Total Catalyst Demand 2,200 m<sup>3</sup>
  - NPV \$7,787,000

# Reagent Consumption

- SNCR NSR 1.4 to 2 Depending On  $\text{NO}_x$  Removal Efficiency
- SNCR + Catalyst Has Higher Reagent Demand Than SCR
- LNB/OFA + SNCR + Catalyst Has Lower Reagent Demand Than SCR

# Pressure Drop

- ASCR Pressure Drop Is 4 To 6 iwg  
Lower Than SCR

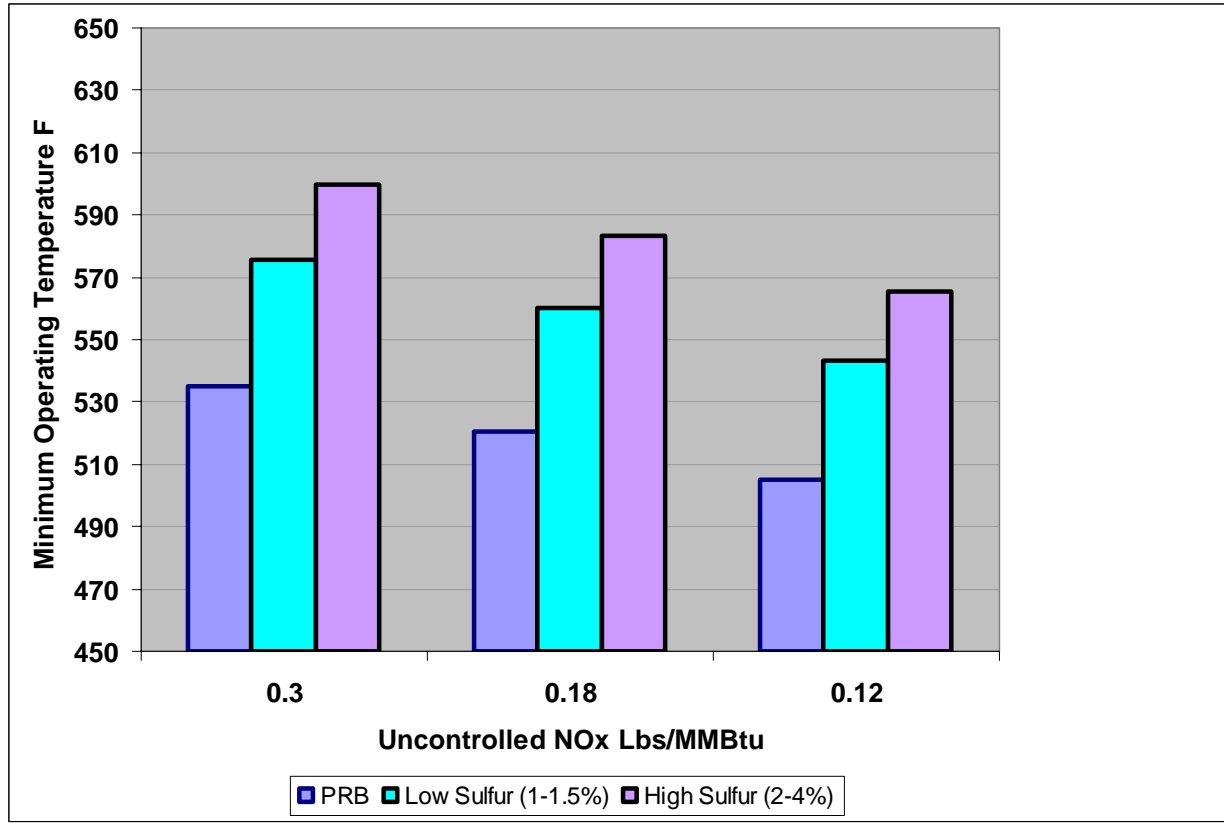
# Reasons For Combination Of Technologies

- Lower Electricity Demand Due To Current Economical Situation
- Political Reason: Global Warming/ Renewable Energy
  - Example: UK plans For 25 % Electricity From Off-Shore Wind Farms By 2030
- Broader Operating Range Required
- Less Total Cost: Poland

# ASCR Challenges

- Physical Space
- Outage Time
- Flow Distribution

# ASCR Operating Range



# China, Light and Power Castle Peak B Units 1-4



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# China, Light and Power Castle Peak B Units 1-4

- Four 685 MW Units
- “Two Shift” Operation
- BOFA/In-Duct Catalyst Retrofit
- More Than 50 % NO<sub>x</sub> Reduction
- Potential For Higher Reduction With SNCR Retrofit
- Catalyst Face Design Velocity 25 fps
- OEM Doosan Babcock

# China, Light and Power Castle Peak B Units 1-4

- Fuel Tech Scope
  - CFD
  - Experimental Model
  - AIG Design
  - Mixer Design
  - GSG Design
  - Ash Screen Design

# China, Light and Power Castle Peak B Units 1-4

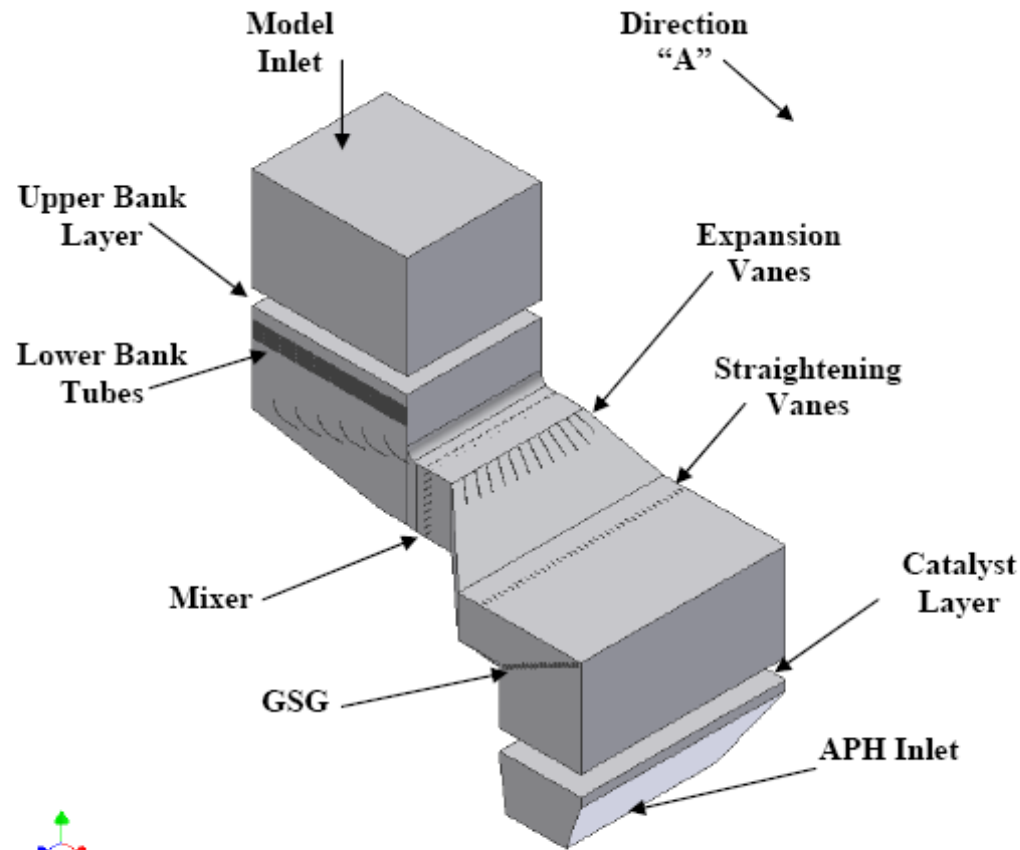


Figure 5: CFD model of Economizer to APH System

# China, Light and Power Castle Peak B Units 1-4

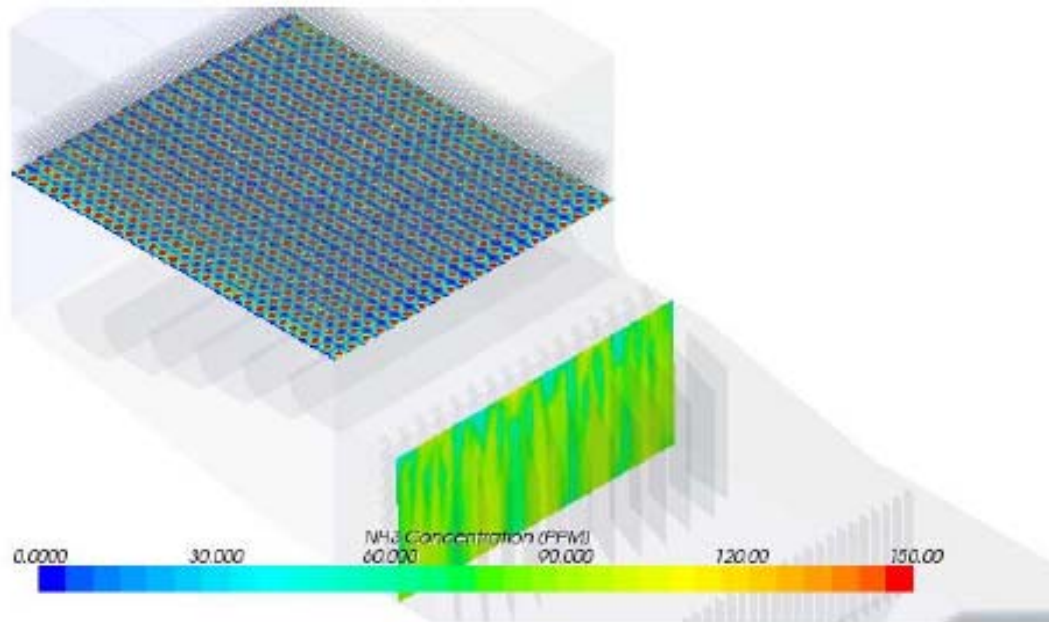


# China, Light and Power Castle Peak B Units 1-4

	Goal	CFD				Experimental			
	+/- 10%	RMSE	+/- 10%	+/-15%	+/- 20%	RMSE	+/- 10%	+/-15%	+/- 20%
Velocity at Catalyst	100%	5.10%	96%	100%	100%	5.8%	94%	98%	100%

	Goal		CFD				Experimental			
	+/- 5%	+/- 10%	RMSE	+/- 5%	+/-10%	+/- 15%	RMSE	+/- 5%	+/-10%	+/- 15%
NH <sub>3</sub> at Catalyst	90%	100%	4.10%	85%	98%	100%	2.96%	90%	100%	100%
NH <sub>3</sub> /NO <sub>x</sub> Ratio at Catalyst	90%	100%	4.39%	83%	98%	100%				

# China, Light and Power Castle Peak B Units 1-4



# China, Light and Power Castle Peak B Units 1-4

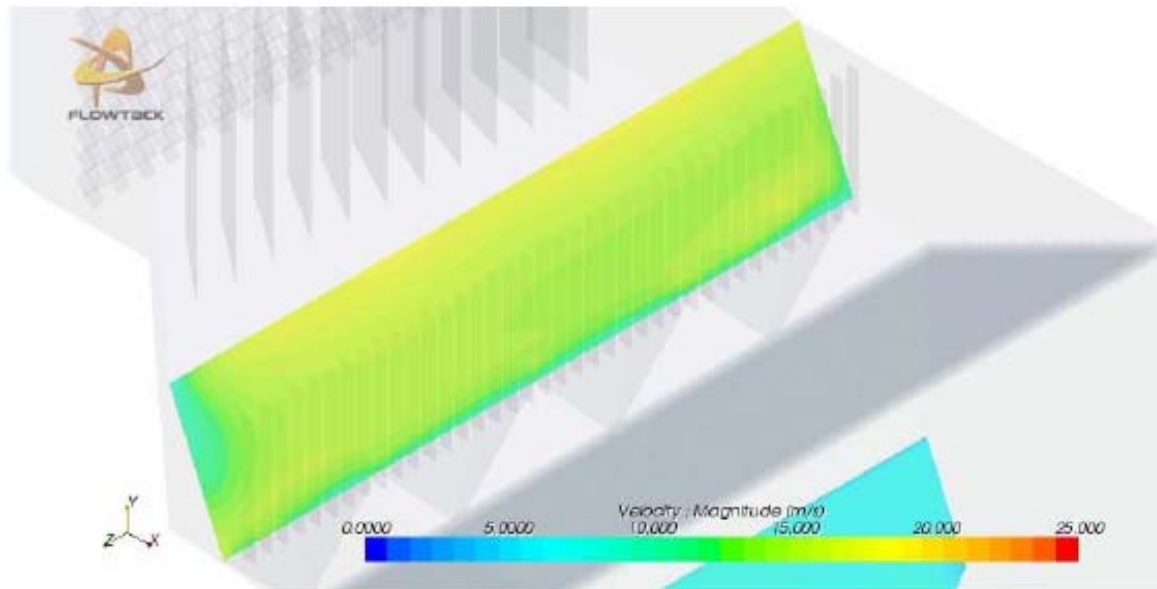
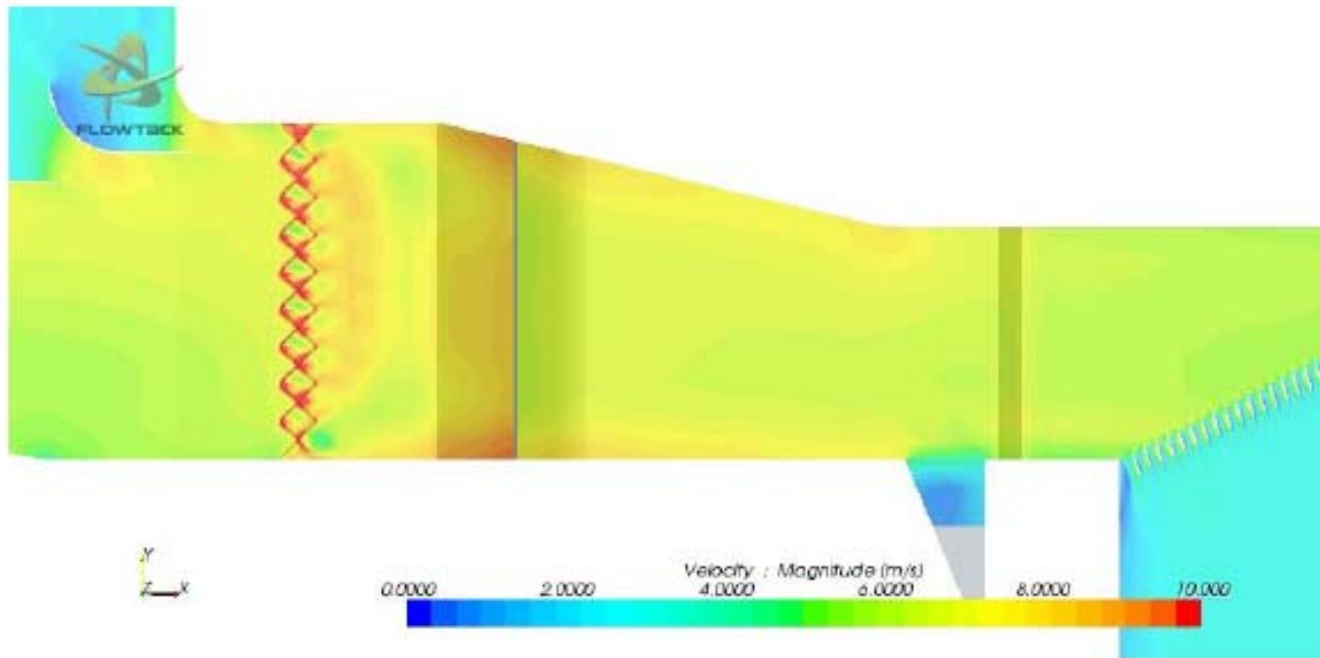
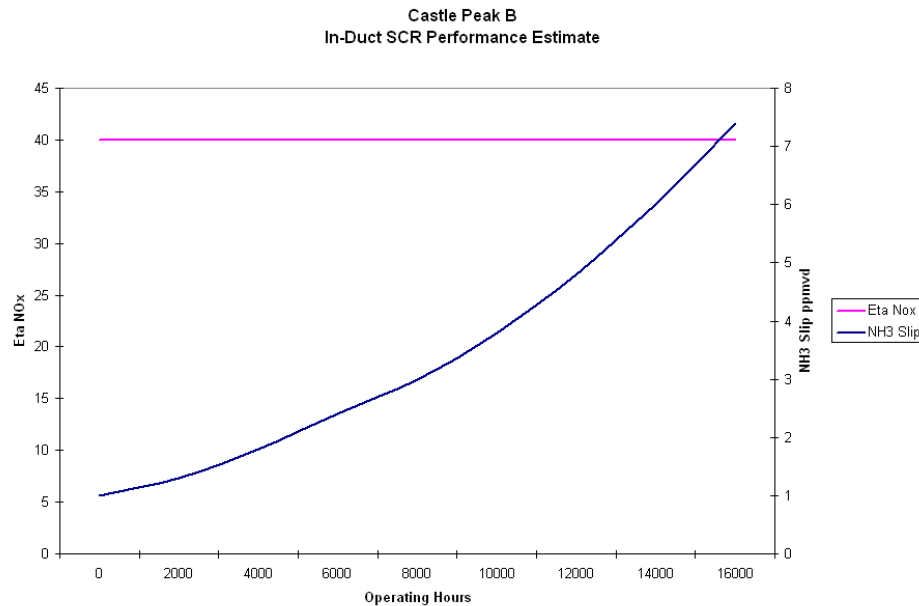


Figure 15: Full Load Velocities at Potential LPA Screen Location

# China, Light and Power Castle Peak B Units 1-4



# China, Light and Power Castle Peak B Units 1-4



# China, Light and Power Castle Peak B Units 1-4

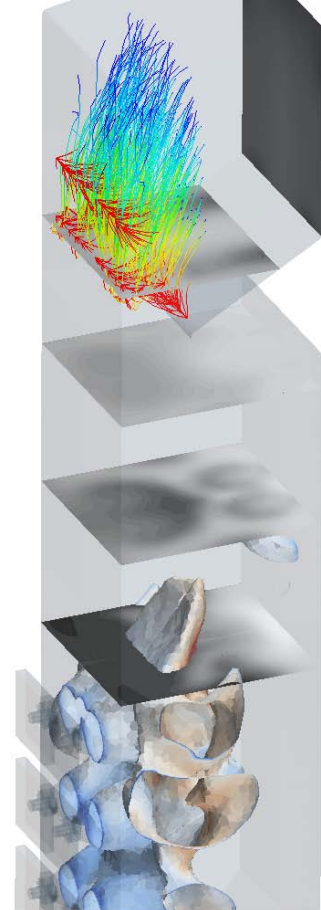
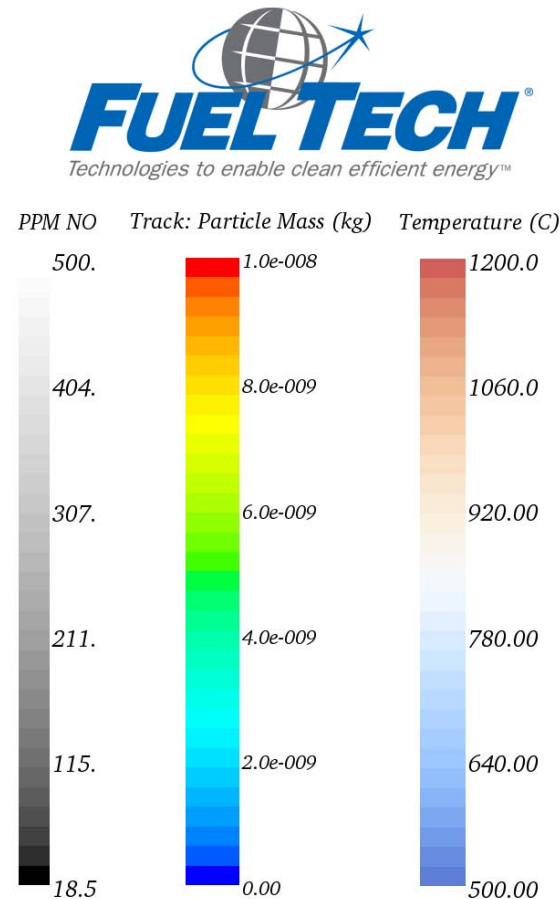


# Current Status

- First Unit Is In Operation
- The Unit Passed The Performance Test
  - NO<sub>x</sub> Reduction Guaranteed At Beginning of Life Time 40 %, Achieved 42 %
  - Ammonia Slip Guaranteed At Beginning of Life Time 3 PPM, Achieved 2.5 PPM

# ASCR CFD Study

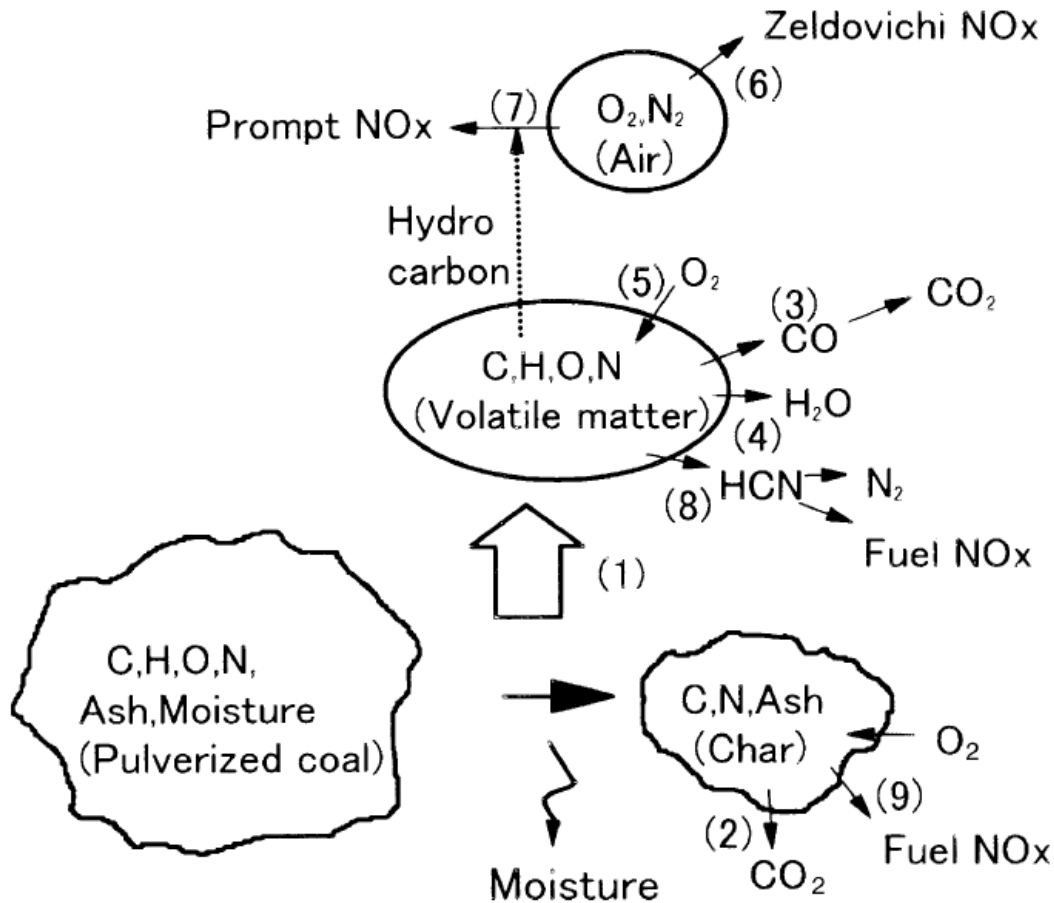
- Computational modeling necessary during design phase for any retrofit installation
- Provides proof of concept NO<sub>x</sub> reduction predictions
- Combustion Modifications + SNCR + SCR



# Products of Combustion

Kurose et al.

- Coal



# Products of Combustion

Zhou et al.

- Pyrolysis
  - Product are fuel dependent

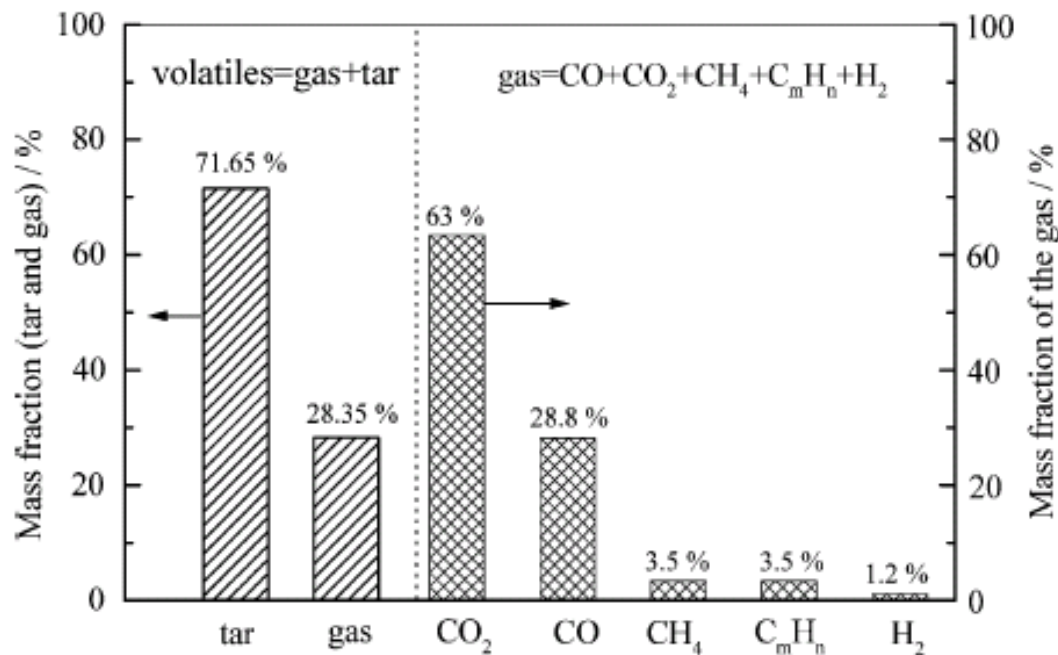


Fig. 2. Yields of pyrolysis products (dry basis).

# Coal Combustion Modeling Basics

- Lagrangian particle tracking
- Drying by Clausius-Clayperon
- Pyrolysis obeys Arrhenius rate and produces tar, light volatiles, char and ash per literature, per fuel
- Tar and light volatile oxidation per Arrhenius rates in literature
- Char combustion controlled by mixed gas film diffusion and chemical reaction
- Fuel N: Volatile HCN / Volatile NH3 / Char N per literature, per fuel
- Fuel and Char N oxidations controlled by Arrhenius rates, per reduced mechanism in literature
- +Zeldovich (Thermal) NOx

Plus NOx creation  
and destruction

# ASCR Test Case: Combustion Mods Design

- 32 MW, B&W front wall-fired unit with 6 burners
  - 29,334 lb/hr Coal; 372,187 lb/hr Air (14% excess)
  - Coal Heating Value: 11,291 BTU/lb
  - Primary/secondary/OFA splits
    - Primary: 63,510 lb/hr (17.1%)
    - Secondary: 234,239 lb/hr (62.9%)
    - OFA: 74,438 lb/hr (20%)
  - Baseline NO<sub>x</sub>: 0.42 lb/mmBTU
- ASCR Design
  - Combustion Mods: 21% removal (0.33 lb/mmBTU)
  - SNCR: 20% removal (0.26 lb/mmBTU)
  - SCR: 25% removal (0.195 lb/mmBTU)
  - Total: 53.5% removal

# Boiler Geometry

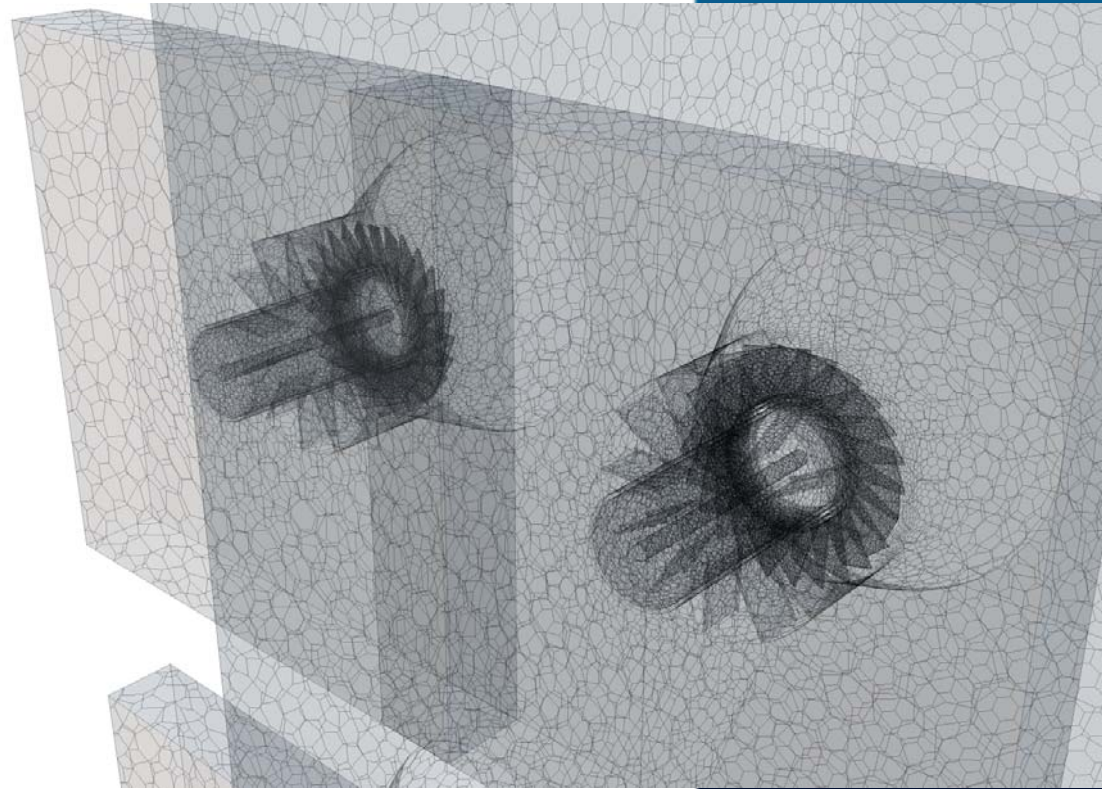
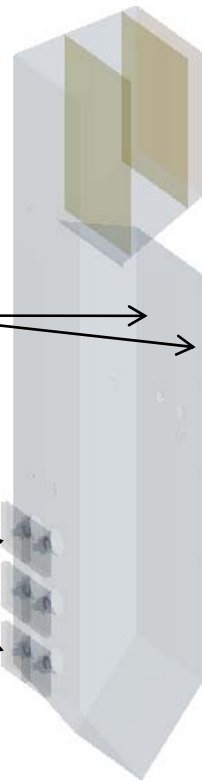
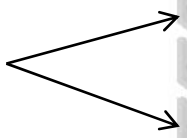
>7 million  
computational cells



OFA  
Ports



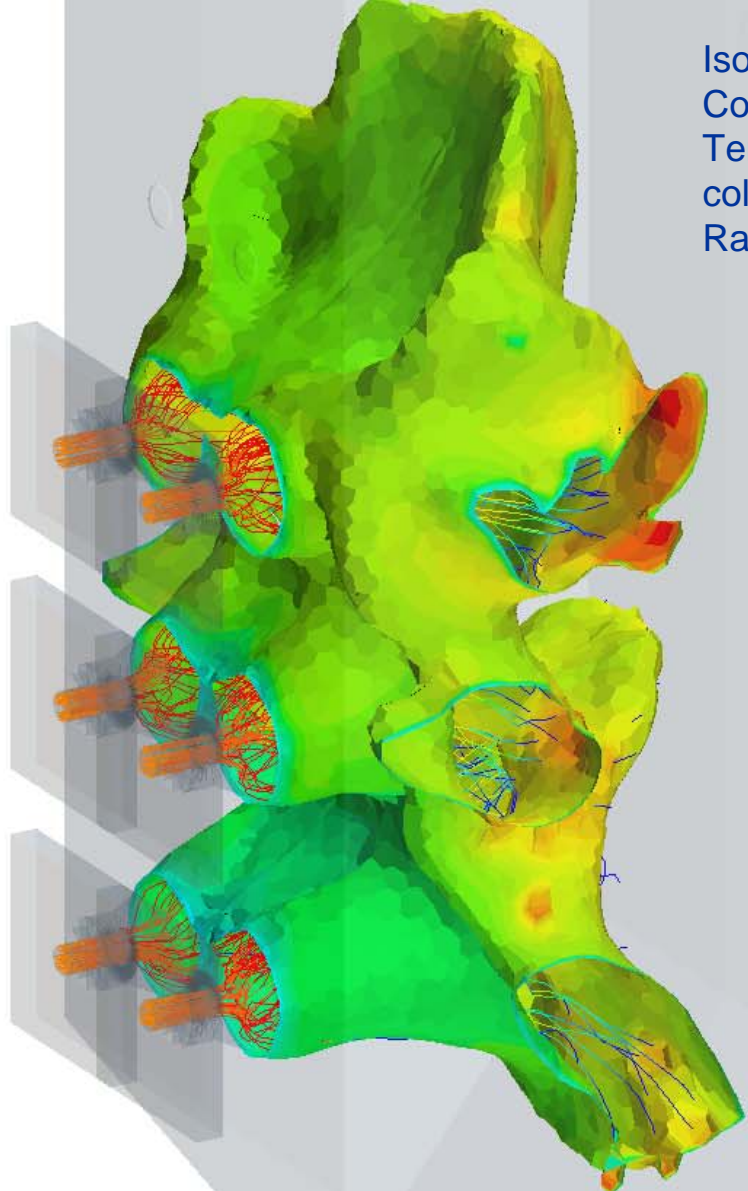
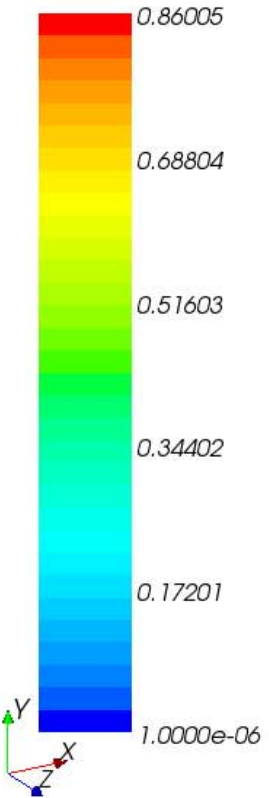
FTI  
LNBS



# Baseline Case

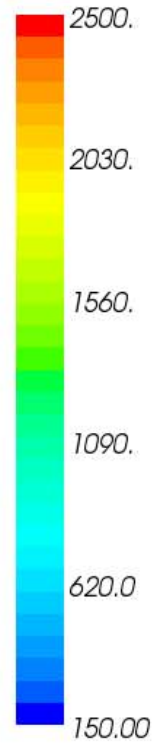


Track: Particle Mass Fraction of RawCoal



Isosurface of 70,000 PPM CO<sub>2</sub>,  
Contours colored by  
Temperature, Coal particles  
colored by Mass Fraction of  
Raw Coal

Temperature (F)

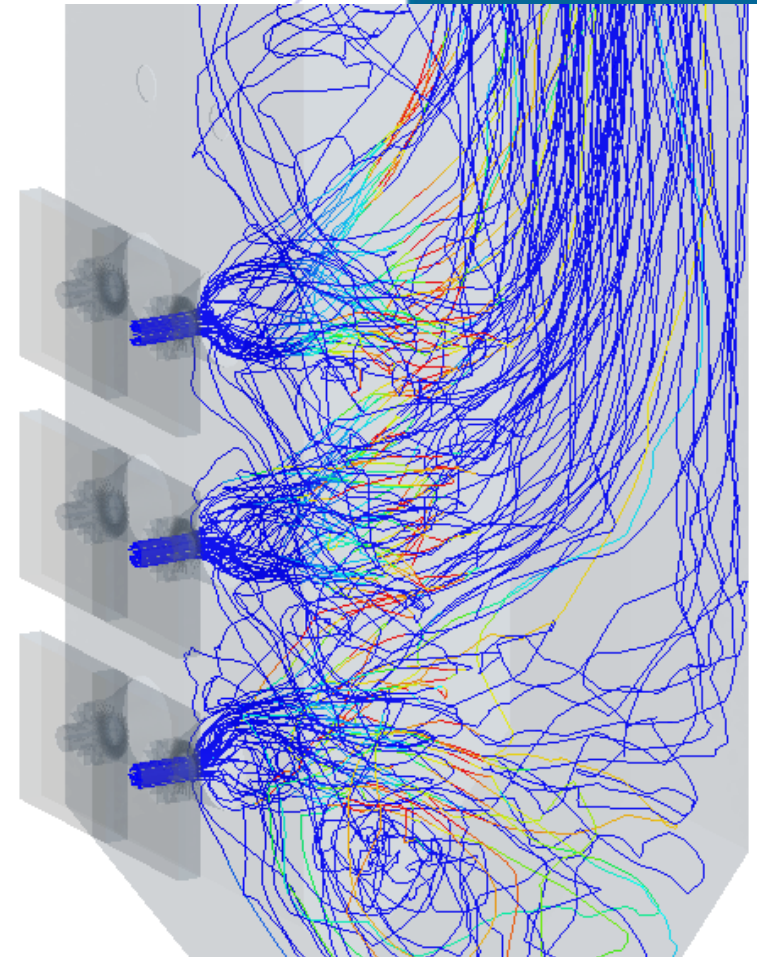
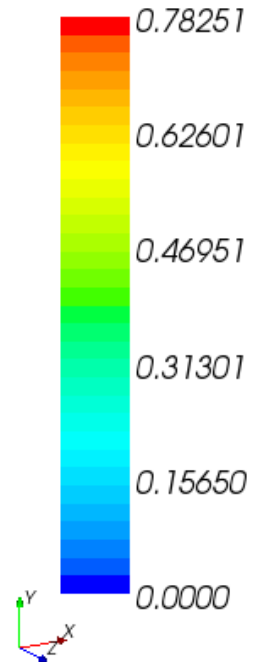


# Baseline Case

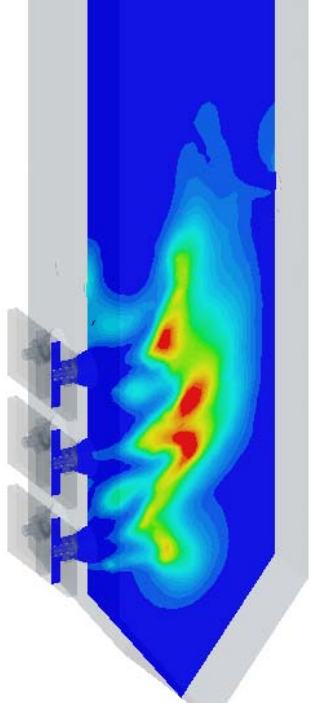
- Coal Particle Char Mass Fraction



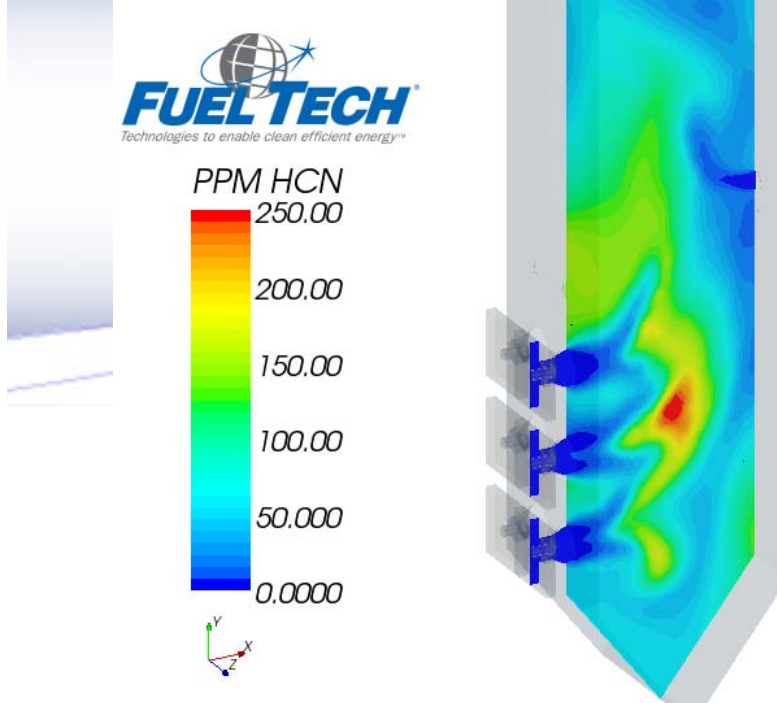
Track: Particle Mass Fraction of Char



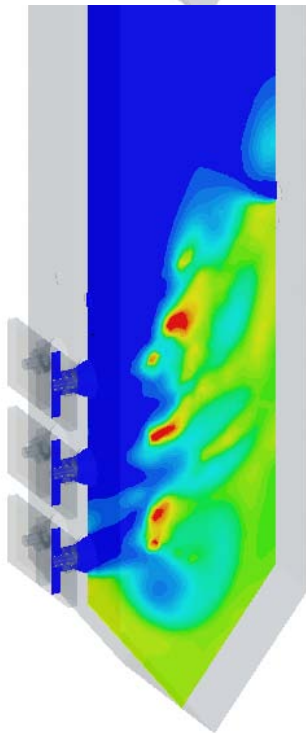
PPM NH<sub>3</sub>  
10.000  
8.0000  
6.0000  
4.0000  
2.0000  
0.0000



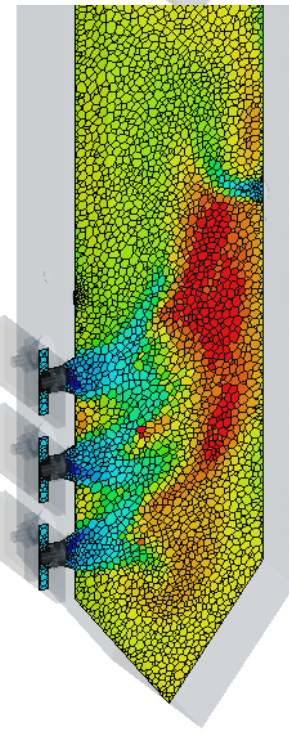
PPM HCN  
250.00  
200.00  
150.00  
100.00  
50.000  
0.0000



PPM CO  
1.0000e+05  
80000.  
60000.  
40000.  
20000.  
0.0000



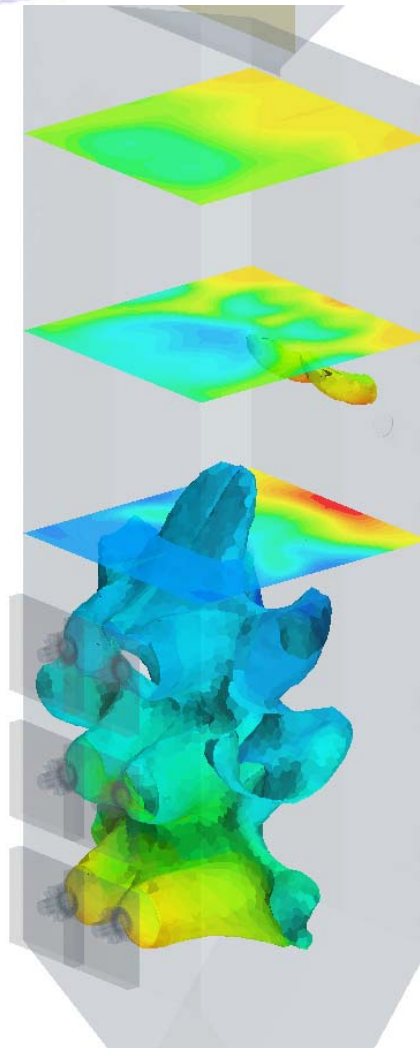
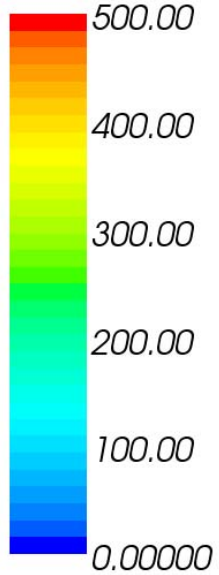
Temperature (F)  
2500.0  
2030.0  
1560.  
1090.0  
620.0  
150.00



# Combustion Mods



PPM NO



# Combustion Mods Results

- Critical Stats
  - Temperature @ Nose: 1840 F
  - Avg. PPM CO @ Outlet: 64
  - Avg. PPM NO @ Outlet: 297
  - 21% NO Reduction

# SNCR Design

- SNCR Design: 20% Reduction from 0.33 lb/mmBTU NO<sub>x</sub> to 0.26 lb/mmBTU
- 34 injectors
- NSR = 3.0 for initial simulation
- Equal flow to each injector (un-tuned) for initial simulation

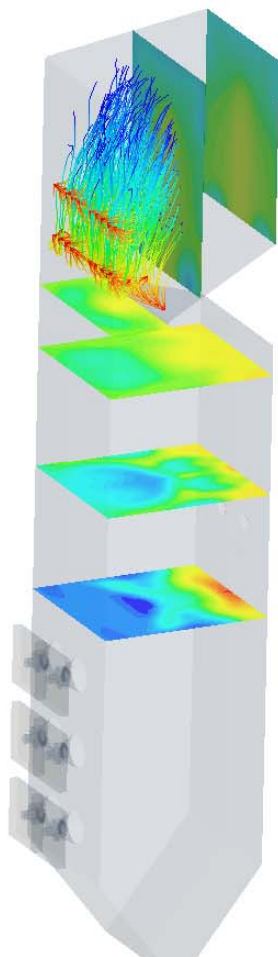
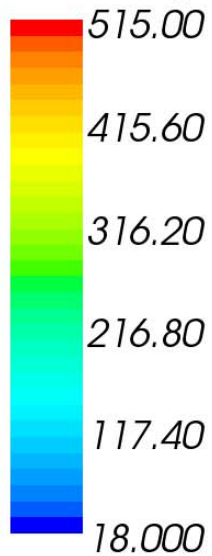
# SNCR Modeling Basics

- Lagrangian particle tracking
- Droplet evaporation by Clausius-Clayperon
- NOx reduction and creation reactions obey Arrhenius type reaction rates, per literature and FTI rates

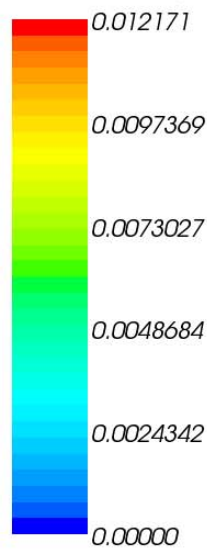
# SNCR Results



PPM NO



Track: Particle Mass (Milligrams)



# SNCR Results

- Critical Stats
  - Avg. PPM NO @ Nose: 297
  - Avg. PPM NO @ Superheater Outlet: 256
  - 14% NO Reduction

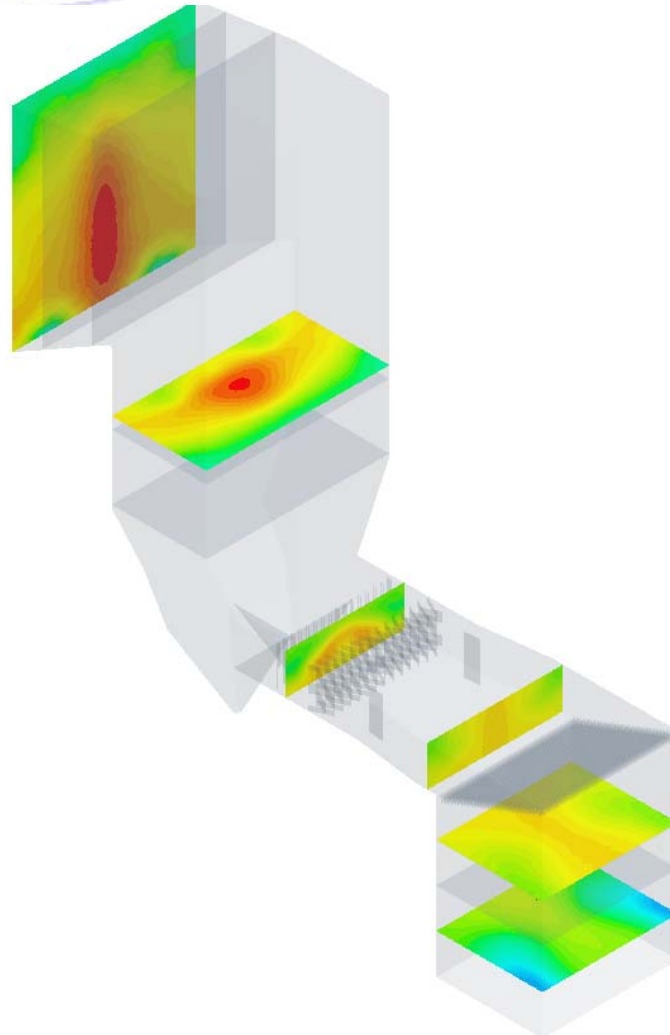
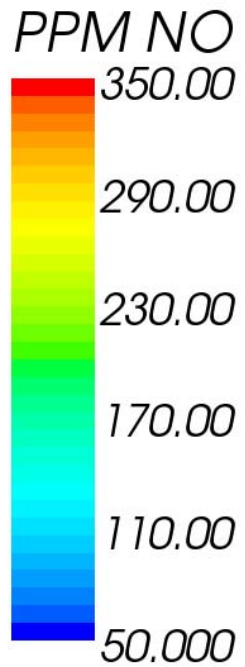
# SCR Design

- 25% Removal from 0.26 lb/mmBTU to goal of 0.195 lb/mmBTU
- Single catalyst layer
- Mixer
- Ammonia Injection Grid (AIG)
- Graduated Straightening Grid (GSG)
- Goal:  $\text{NH}_3$  slip to 2 ppm average leaving SCR

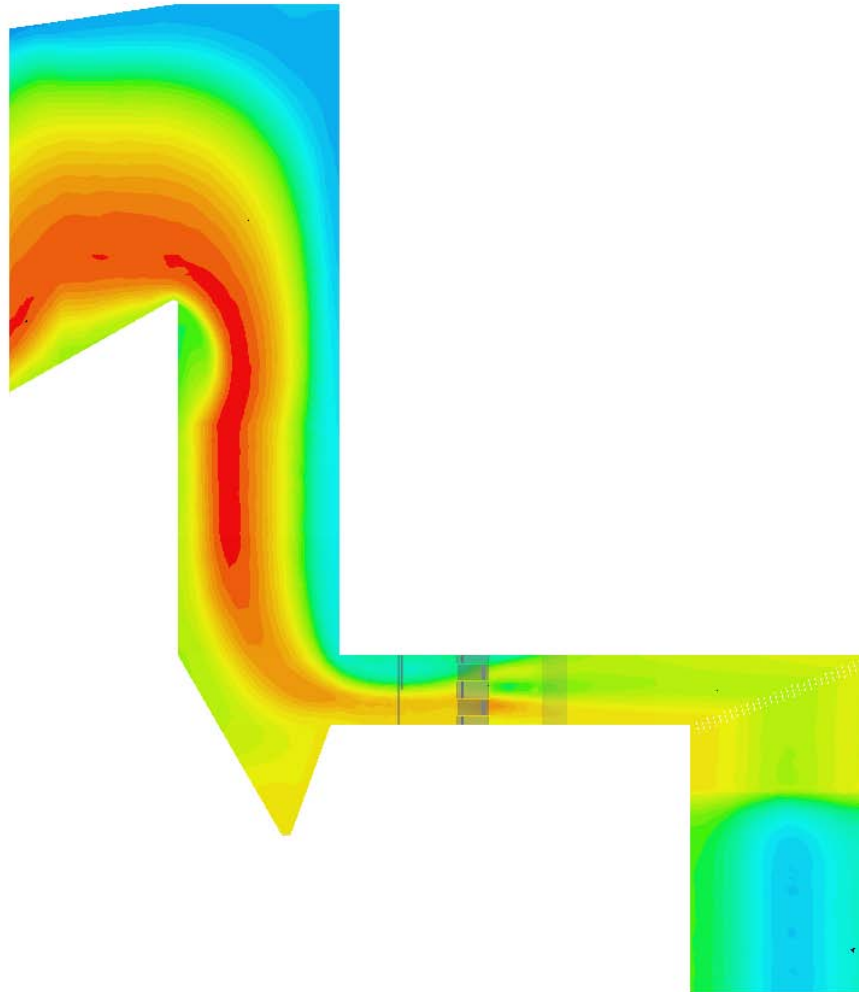
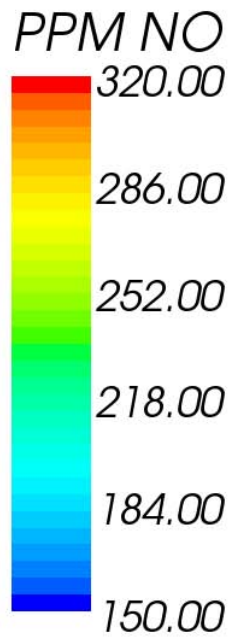
# SCR Modeling Basics

- NO<sub>x</sub> reduction reaction obey Arrhenius type reaction rates, per literature and FTI rates

# ASCR Test Case



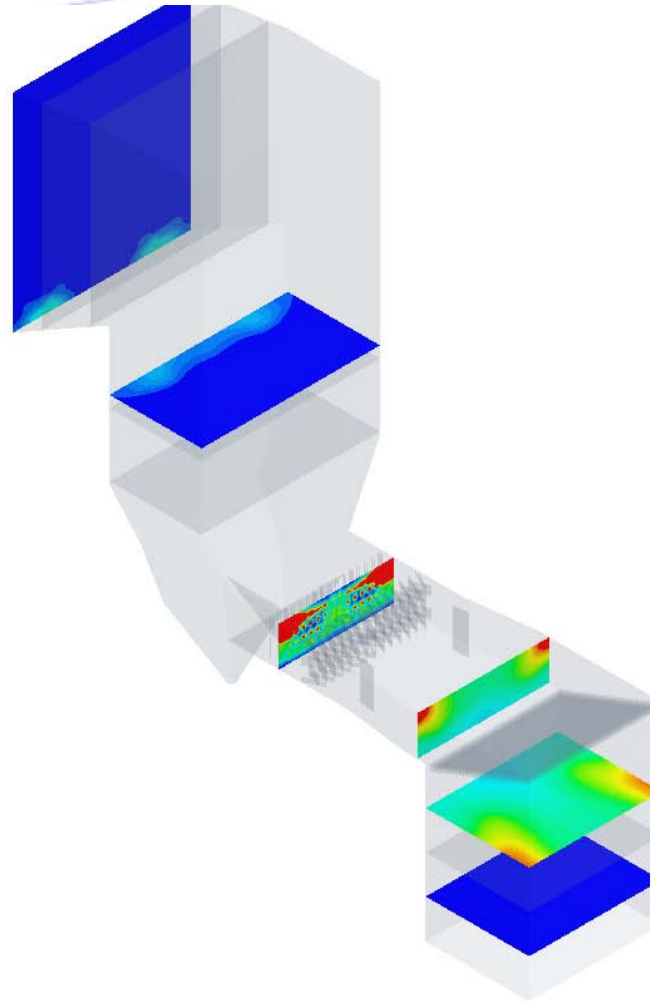
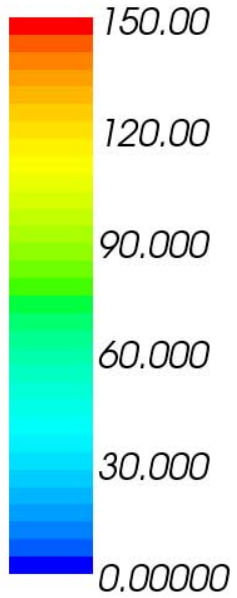
# ASCR Test Case



# ASCR Test Case



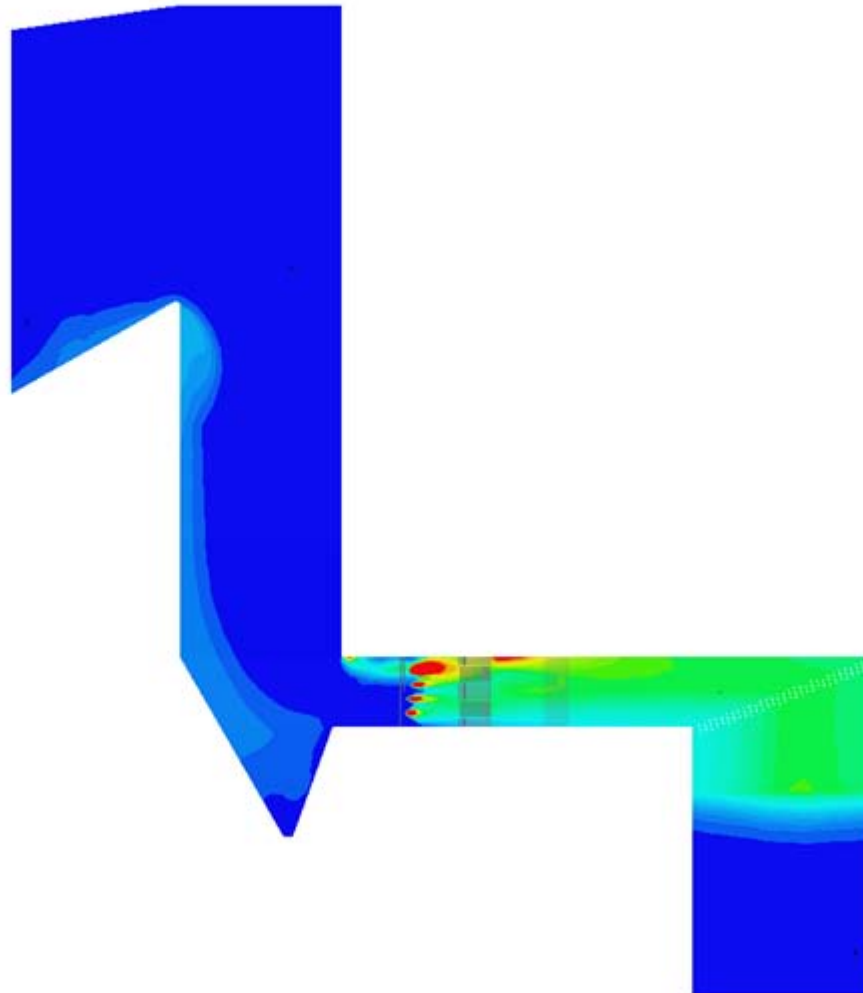
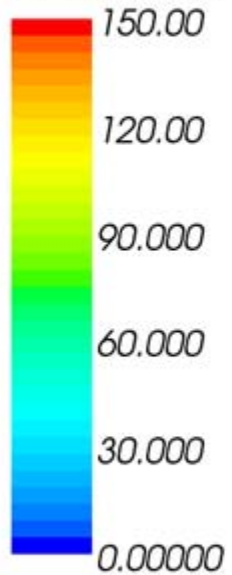
PPM NH<sub>3</sub>



# ASCR Test Case



PPM NH<sub>3</sub>



# SCR Results

- Critical Stats
  - Avg. PPM NO @ SCR Inlet: 297
  - Avg. PPM NO @ SCR Outlet: 256
  - 24% NO Reduction

# ASCR

## Test Case

- Baseline NO: 378 PPM (0.42 lb/mmBTU)
- NO At Furnace Nose: 297 PPM (.33 lb/mmBTU)
  - Combustion Mod Removal = 21%
- NO After SNCR Zone: 256 PPM (.285 lb/mmBTU)
  - SNCR Removal Efficiency: 14% (Un-tuned)
- NO Downstream Catalyst: 195 PPM (.217 lb/mmBTU)
  - Catalyst Removal Efficiency: 24% (Un-tuned)
- Total Removal = 48%
- NH3 Slip at Model Outlet: 1.5 PPM